

Infrarot-Bildwandlerröhre AEG B 80 S

Anwendung: Umwandlung von Infrarot-Strahlung in sichtbares Licht. Triode mit elektrostatischer Fokussierung ohne eingebauten Spannungswandler. Nutzbarer Kathodendurchmesser 26mm. Nutzbarer Leuchtschirmdurchmesser 23mm.
Röhrensystem--Triode
Fokussierung--elektrostatische Fokussierung
Photokathode---halbtransparent
Maximum der spektralen Empfindlichkeit ca. 800 nm
langwellige Grenze der spektralen Empf. ca 1200nm



	max.	min.	
A	88,8	87,2	mm
C	80,8	79,2	mm
D	41,9	-	mm
E	40,1	-	mm
F	21,8	-	mm
G	64,0	59,0	mm
M	-	23,0	mm
N	-	26,0	mm
P	34,15	33,85	mm
Q	36,25	35,95	mm
U	5,5	4,75	mm
X	3,5	2,75	mm

Der Brechungsindex des Glases der Kathoden- und Schirmscheibe ist 1,5.

The refractive index of the glass of the cathode- and screen window is 1.5.

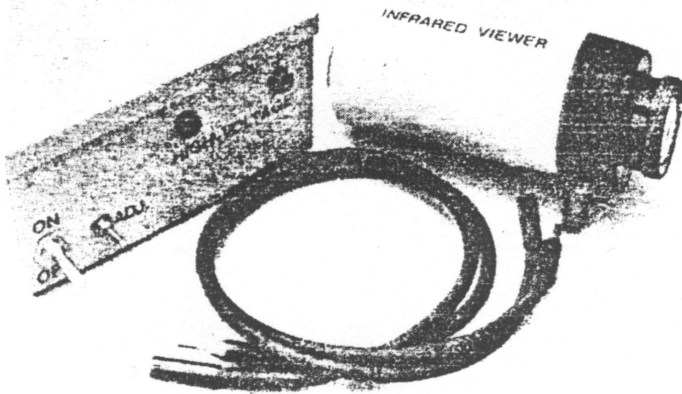
Anodenspannung + 16 KV, maximum + 17 KV, Fokusspannung + 3 KV, Maximum + 4KV ,

Dunkelstrom <0,02 uA, Vergrößerung typ. 0,72

Betrieb: Falschpolung der Betriebsspannung kann auch bei nur kurzzeitigem Betrieb zur Beschädigung bzw. Zerstörung der Photokathode führen. Zu hohe Lichtbelastung der Photoempfindlichkeit kann zum vorzeitigen Abfall der Photoempfindlichkeit und zu Einbrennflecken führen.

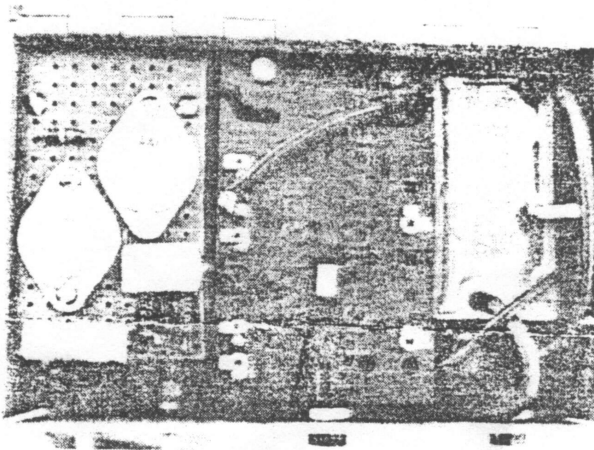
Die Röhre soll nur mit einem Infrarotfilter vor der Photokathode betrieben werden.

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COMPLETE IR VIEWER (left) and a 6032 image tube (above) with voltage divider added. Power supply connections are high-voltage cable.

Bildwandlerröhre



Infrared technology has made rapid strides in surveillance, security, ecological surveys and other fields. This simple experimental viewer has many applications.

by FORREST M. MIMS

INTERNAL VIEW of image tube power supply. Oscillator is at left, T2 at center and voltage tripler at right. Never open supply housing when operating and never operate supply without a load.

INFRARED EMITTING LASERS AND LED'S ARE of great value in light beam communicators, intrusion alarms, and ranging systems. All these applications, however, would be easier to achieve if the invisible beam from the infrared source could be seen during alignment.

Phosphor viewing screens are available for as little as \$25, but they suffer from low resolution and limited viewing time before requiring "recharging" from an ultraviolet source. The next least expensive solution is an infrared image converter tube, but even war surplus tubes with an integral power supply cost \$300 or more.

An ideal solution to the problem is to assemble the infrared image converter described here. This device is centered around a variable-output high-voltage power supply capable of operating practically any new or surplus image tube.

and this permits an entire image conversion system to be put together for a tenth the cost of the least expensive commercial units.

How it works

Image converter tubes contain a light-sensitive photocathode which emits electrons when struck by light. Various cathode coatings are available for ultraviolet, visible, or infrared light. An anode surrounding a

phosphor coated viewing screen is connected to a positive high voltage and attracts electrons emitted by the photocathode. As the electrons strike the phosphor screen, they excite individual phosphor atoms to higher than normal energy levels. When the atoms resume equilibrium, they emit a yellowish-green light.

Some image tubes require electrostatic focusing and include a central grid for the purpose. The 6032 is an example of an electrostatic focused tube. More recent tubes, such as the 6929, include prefocused internal grids and are easier to operate. Self focused tubes such as the 6929 will operate from about 12 kilovolts, while the 6032 requires a hefty 20 kV.

Too much voltage can damage or destroy an image tube, so a power supply designed to operate a variety of tubes must have a variable voltage control. The very high voltage required for the tube can be generated by several techniques. Since the image tube may be required to operate from batteries in such field applications as aligning an infrared communicator or intrusion alarm, the system should be capable of low voltage operation. In-house operation of the tube, however, is best accomplished by means of 117 Vac. For this reason a compromise circuit permitting both modes of operation at the least possible expense was chosen.

The circuit diagram for the power supply is shown in Fig. 1. In operation, transformer T1 and the rectifier bridge convert the 117 Vac delivered by the household line to 11 volts of pulsating dc. Filter capacitor C1 smoothes this voltage and passes it on to a regenerative amplifier composed of Q1 and Q2.

The regenerative action of Q1 and Q2 causes an oscillation with pulses of dc at near the power supply voltage being delivered to the primary of high-voltage flyback transformer T2. R1 varies the voltage output of the oscillator and serves as a variable high voltage control. The dc pulses from the oscillator are converted to ac by the inductor action of T2's primary. T2's inductance causes the dc pulses switched by Q2 to have an undershoot nearly as great in amplitude as the pulse itself.

T2 has a very high turns ratio so a small voltage at its primary is stepped up to a high voltage at its secondary. The high-voltage output of T2, which ranges up to about 14 kV depending on R1's setting, is smoothed and increased by a factor of three by voltage tripler VT1. The output of the tripler is connected to the image tube.

Putting it together

Construction of the high-voltage power supply would be straightforward.